TIME SHIFT DATA ANALYSIS FOR
LONG-RANGE GUIDED WAVE INSPECTION

TECHNICAL FIELD OF THE INVENTION

This invention relates to non-destructive testing, and more particularly to the use of long-range guided waves for such testing.

BACKGROUND OF THE INVENTION

Nondestructive testing has proven to be an essential tool for assessing corrosion and erosion related damage in large equipment and structures. For long lengths of structure, such as pipes, tubes, steel cables, and plates, long range guided wave inspective has proved to be effective. Using long range guided wave techniques, a long length of structure can be inspected quickly and economically from a given probe location.

One example of a long range guided wave technique is an ultrasonic technique based on the use of Lamb waves. The guided waves are generated by using piezoelectric probes and mechanically coupled into the material under inspection. The Lamb waves propagate between two parallel surfaces and can be used to detect changes in wall thickness. This technique is described in U.S. Patent No. 6,148,672, to Cawley, Alleyne and Chan, entitled "Inspection of Pipes," assigned to Imperial College of Science, Technology of Medicine (London).

Another example of a long range guided wave technique uses magnetostrictive probes. These probes generate and detect mechanical waves in ferromagnetic material. Testing of a pipe involves two sets of an inductive coil encircling the pipe and a bias magnet. A time-varying magnetic field is applied to the pipe by the transmitting coil and this generates an elastic wave in the pipe due to the magnetostrictive effect. The waves propagate along the pipe in both directions. The receiving magnetostrictive probe uses the other encircling coil to detect changes in magnetic induction in the pipe due to the inverse magnetostrictive effect

when the waves pass through. The system does not require
a couplant or direct contact. This technique is
described in U.S. Patent No. 5,581,037, entitled
"Nondestructive Evaluation of Pipes and Tubes Using
5   Magnetostrictive Sensors," to Kwun and Teller, assigned
to Southwest Research Institute (San Antonio, Texas).

Guided waves can exist in various modes, such as
longitudinal, flexural, and torsional wave modes in pipe
or tube, and symmetric and antisymmetric Lamb wave and
10   shear horizontal wave modes in plate. In each wave mode,
they can exist in different forms, with the forms
referred to as "orders". Guided waves are also
dispersive, and therefore, their velocity of propagation
varies with wave frequency.

15   To simplify analysis of the detected signals, the
probes for long range guided waves are often controlled
to generate a single wave mode of a fixed order that is
propagated in a given direction, and to detect the same
wave mode traveling in the opposite direction after
20   reflection from a defect or a normal geometric feature
such as a weld.

In practice, the control of wave mode and
directionality is imperfect. As a result, extraneous
wave modes are generated and detected, and extraneous
25   waves may be propagated in directions other than the
intended direction. These extraneous signals can be
confused with the desired reflected signals, leading to
erroneous data interpretation. Because of the
complexities of guided waves, as well as of geometric
30   features in structures, proper analysis of acquired data
is time consuming and requires extensive knowledge of

guided wave properties and interactions with geometric
features in the structure.

SUMMARY OF THE INVENTION

One aspect of the invention is a method of analyzing long range guided wave data to identify signals of the intended wave made of a fixed order that are reflected from defects and geometric features in the intended direction. Two sets of reflection signals are acquired. The first data set is acquired from a first probe position. The second data set is acquired from a second probe position having a known separation from the first probe position. Signals whose amplitude exceed a pre-determined threshold value are then identified from both sets of data. Next, the signals in one set of data values are time-shifted by an amount that would cause the signals to occur at the same time if the probes were in the same position. The shifted data values are compared to the unshifted data values to determine any coincidence in time between two signals. Signals that coincide are interpreted as representing the correct signals that are reflected from defects and geometric features in the intended direction. Signals that do not coincide are interpreted as representing extraneous signals.

An advantage of the invention is that it provides simple and accurate data analysis of long range guided waves. The method identifies primary wave mode signals and excludes extraneous signals. The analysis is automated in a manner that permits the data to be interpreted quickly without requiring a high level of knowledge of the guided waves.

BRIEF DESCRIPTION OF THE DRAWINGS

FIGURE 1 illustrates a system for time-shift checking of guided wave data in accordance with the invention.

5   FIGURE 2 illustrates the method implemented by the system of FIGURE 1.

FIGURE 3 illustrates the two data sets acquired from the two probe positions described in FIGURE 1.

FIGURE 4 illustrates the data sets of FIGURE 3, with
10   signal amplitude values exceeding a threshold identified.

FIGURE 5 illustrates the identified signal values of FIGURE 4, with further identification of signal values in the second set that are within a specified time limit of signal values in the first set.

DETAILED DESCRIPTION OF THE INVENTION

　　　　FIGURE 1 illustrates a system 10 for analyzing guided wave data in accordance with the invention. The reflected signals are detected from two probe

5　positions 11 separated by a short distance apart. As discussed in the Background, there are various approaches to long range guided wave testing, and various types of probes may be used for such testing. Examples of suitable probes are those used for Lamb wave inspection

10　or those used for magnetostrictive testing. In the example of FIGURE 1, the probe at each position is of a type appropriate for magnetostrictive testing and encircles pipe 12. A suitable separation distance, d, between probe positions 11 is four inches.

15　　　　The probe outputs are delivered to a processing system 13, which has memory and processing components suitable for implementing the method described herein. Processing system 13 is programmed with instructions for carrying out the algorithms described below, and may

20　further be programmed with suitable user interface for receiving operation commands and displaying results to an operator.

　　　　　Time Domain Data Analysis

25　　　　FIGURE 2 illustrates the method implemented by the system of FIGURE 1. Essentially, as explained below, the method involves acquiring two sets of data, one set from each probe position 11. Signals whose amplitude is above a pre-determined threshold value are identified from each

30　set. Then, the identified signals in one set are time-

shifted, and their shifted occurrence times are compared
against those in the other set.

The method may be implemented with either time
domain or frequency domain data. The method of FIGURE 2
5 is first described herein in terms of time domain data.

Step 11 is acquiring two sets of guided wave data,
each set from a different probe location, with the
locations separated by a short distance. For time domain
analysis, the two sets of data may be A-scan data,
10 characterized by use of a pulse or tone burst, which is
output by a probe and either received by that same probe
(pulse echo) or another (pitch catch). The waveform
amplitude is plotted versus time.

FIGURE 3 illustrates an example of two sets of A-
15 scan guided wave data from probes 11 placed at two
different locations on structure 12. Each set of data is
represented by a plot of signal amplitude (volts) against
time (milliseconds). The total test time in this case is
14 milliseconds (corresponding to the round-trip time of
20 the longitudinal wave over an approximately 39-meter long
pipe), and the range of signal values is within a range
of 1 to -1 volts.

Step 13 is identifying signals in both data sets
whose amplitude exceeds a certain threshold. The
25 threshold value is chosen to be at least twice the
background noise level in the data. The actual threshold
value used in the algorithm is determined by the operator
based on the desired level of defect delectability (for
example 20 percent of a weld signal amplitude).

30 Various algorithms may be used for implementing Step
13. An example of an algorithm for finding signals whose

amplitude exceeds the threshold is begun by first
specifying the length of a "gate" to be used. A suitable
gate length is one approximately equal to the pulse
length of the signal. The signal is then examined within
5   the gate length to determine the maximum signal
amplitude, V_i, ($i = 0, 1, 2, . . .$numbered consecutively
from the first signal identified)within the gate length.
If V_i exceeds the threshold, then its occurrence time, t_i,
is recorded. Otherwise, the data in that gate length is
10 ignored. A number of initial data points from time t =
0, where the initial pulse occurs, may be ignored so as
to avoid calling signals caused by the initial pulse.

     Successive values of V_i are identified by moving the
gate by half gate-length increments, and in each new gate
15 length, determining a maximum value and comparing that
value to the threshold. The half-gate length increments
are repeated until the end of the data file. The result
is a set of maximum amplitude values, each having an
associated occurrence time. For each maximum amplitude
20 value, its occurrence time, t_i, is compared with the rest
of the data point times. Expressed mathematically, each
t_i is compared with all other occurrence time values, t_j,
where j is a value from 1 to n and n is the time of the
last point in the data. If $|t_i - t_j|$ is greater than the
25 gate length, then the corresponding amplitude value is
chosen for time-shift checking. If $|t_i - t_j|$ is less than
or equal to the gate length, this implies more than one
amplitude value within a gate and only the corresponding
amplitude value within the gate having the maximum
30 amplitude is chosen for time-shift checking. This
process of incrementing by half gate lengths and

comparing occurrence times is designed to best locate
maximum values while avoiding duplicate values. The
result is a set of peak signal values, V_{peak} , and an
associated occurrence time value, within each gate. The

5   peak value occurrence times for the first set of data are
referred to herein as t^1 times, whereas the occurrence
times for the second set of data are referred to herein
as t^2 times.

Next, for each gate length, in addition to a peak

10   value occurrence time, a median occurrence time value is
determined. Within each gate, this is achieved by
identifying the first and last time locations at which
the signal breaks the threshold. Then, the two values
are averaged. The result is two sets of median time

15   values, t'^1 and t'^2.

FIGURE 4 illustrates the data sets of FIGURE 3, with
peak data values identified. In the example of FIGURE 4,
the threshold value was selected to be 0.02 volts of
signal amplitude. For the test data of FIGURE 4, where

20   the pulse frequency is 64 kHz, a gate length of 3/64
milliseconds could be used.

Step 15 is performed for each of the peak signal
values identified in Step 13, in one of the data sets.
For each of these signal values, its occurrence time is

25   time-shifted by an amount equal to the roundtrip time of
the primary guided wave mode over the distance between
the two probe locations. The shifting (addition or
subtraction) is performed in such a way that signals from
a given reflecting feature, such as a weld or defect, on

30   the side of the structure to which the transmitted wave

is directed would occur at the same time in both data
sets.

Step 17 and 19 involve reviewing all the selected
peak values and locating all peak values in the unshifted
5   data set occurring at the same time as peak values in the
shifted data set. Values matching in this manner are
interpreted as representing signals from geometric
features in the structure or defects. Signals not so
matching are interpreted as being caused by extraneous
10   signals and are therefore excluded from further analysis.

An example of an algorithm for implementing Step 17
begins with specifying a time limit within which the
signals in both data sets are considered to occur at the
same time. Typically, this time limit is set to a value
15   to between 1/2f and 1/f, where f is the operating
frequency of the guided wave. Next, time values t^1 and
t'^1 from the data obtained from one probe position are
compared to the time values t^2 and t'^2 from the data
obtained from the second probe position. As indicated
20   above in connection with Step 13, each peak data value
has four associated time values: t^1, t'^1, t^2, and t'^2. If
any one of the following four difference values is equal
to or less than the specified time limit, then the
associated signal value is identified as occurring at the
25   same time in both sets of data: $|t^1 - t^2|$, $|t^1 - t'^2|$,
$|t'^1 - t^2|$, and $|t'^1 - t'^2|$. In other words, the signal
values are "matching". The matching signal values are
considered to represent defects or geometric features in
the structure being tested. If none of the above four
30   values is equal to or less than the specified time limit,

then the signal value is not considered to occur at the
same time in both sets of data, and is therefore ignored.

FIGURE 5 illustrates the same signals as FIGUREs 3
and 4, but with identification of matching signal values,
5   that is, the signal values from one set that are within
the specified time limit of signal values from the other
data set.   These signals are identified as "real"
signals, which indicate defects and geometric features in
the structure (in this case a pipeline).

10   Because of wave attenuation, signals from the same
defects or geometric features decrease in amplitude with
increasing transit-time (or distance to the probe
position).   The constant threshold values used in the
method described in FIGURE 2 mean that the level of
15 defect detectability decreases with increasing time in
the data.   A constant level of defect detectability can
be maintained by either compensating the attenuation
effect on the data or by applying the attenuation to the
threshold value.

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Frequency Domain Data Analysis

For frequency domain data analysis, A-scan data may
be converted to spectrogram data.   A method for this type
of analysis is described in the following article:
25 H. Kwun, K.A. Bartels, and C. Dynes, "Dispersion of
Longitudinal Waves Propagating in Liquid-Filled
Cylindrical Shells," J. Acouset. Soc. Am. 105, pp.
2601-2611, 1999.   To preserve spatial resolution, the
window length used for spectrogram analysis is kept as
30 short as possible but sufficiently long so that
dispersion properties of the waves are observable.

The spectral amplitude at several frequencies is summed. Using the summed spectral amplitude data, the process described above for time domain data is performed. For identifying signals exceeding a threshold
5 (Step 13), the process is performed using maximum spectral amplitudes. An additional step of checking data values on either side of identified maximum values to discard non peak values may be performed. Signals that occur at the same time in both sets of data are
10 identified. The identified signals are then converted back to A-scan data.

Other Embodiments

Although the present invention has been described in
15 detail, it should be understood that various changes, substitutions, and alterations can be made hereto without departing from the spirit and scope of the invention as defined by the appended claims.